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# Multi-robot nonlinear model predictive formation control: Moving target and target absence



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# HIGHLIGHTS

- Proposed a novel approach in formation control and active target tracking problem.
- We consider moving target and the target's presence and absence.
- The NMPFC allows the formation to converge and follow a target or a leader.
- Despite vision problems in real robots, the approach worked successfully.

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# 1. Introduction

A novel adaptive framework based in nonlinear model predictive control was conceived, in this study, and applied to the formation control of a group of mobile robots. A nonlinear model predictive control (NMPC) is used to converge a group of omnidirectional mobile robots (the 5dpo robots seen in Fig. 1) toward a desired target. The formation must be such that allows the movement of robots around the target, avoiding mates and minimizing the total amount of uncertainty in the target's perception of the group. The mobile robots team must also use the NMPC to keep adaptive formation with a moving target. Furthermore, the case of target absence where a leader robot is determined and the other robots in the group follow the leader robot using the NMPC is considered. Finally, the NMPC is implemented in a distributed fashion, embedded in each robot, and exchanging information with the

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ABSTRACT

This paper describes a novel approach in formation control for mobile robots in the active target tracking problem. A nonlinear model predictive formation controller (NMPFC) for target perception was implemented to converge a group of mobile robots toward a desired target. The team must also maintain a desired formation following a target while it is moving, or follow a leader in the case of target's absence. The structure details of the controller, as well as a mathematical analysis of the formation model used, are presented. Furthermore, results of simulations and experiments with real robots are presented and discussed.

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other robots in formation and it is called here nonlinear model predictive formation control (NMPFC).

This work is inserted in the active target tracking [1-4] and formation control problems [5-10]. Therefore, the problem addressed in this paper lies in the frontier between the formation control problem and the active target tracking problem. The problem here is to conceive a formation controller capable of controlling a multirobot system in a distributive fashion considering obstacles and mates avoidance, the formation itself and the maximization of the target's observation by the group of robots in formation.

In formation control, the leader-following approach is one of the most studied [11–20]. It is based on the existence of a leader (real or virtual) that follows the precise desired trajectory while the other robots members of the formation just follow it, maintaining a preset distance and relative position. The leader robot can be a real robot with a different controller and a path generator, or it can be a virtual leader such as a target is in the target tracking problem.

One of the most used controllers in the leader-follower approach is the model predictive controller (MPC). It has been the target of studies about multi-robot motion control for almost a decade

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Fig. 1. The 5dpo robot.

since the first work done by [11]. After that, various works have improved the technique through time, such as [21]. Here, the authors investigated the leader-following formation control of mobile robots through the MPC. They established its control stability by adding a terminal state penalty to the cost function and a terminal state region to the optimization constraints. The authors also designed a terminal state region based on an input–output feedback linearization controller for the MPC. A suboptimal stable solution is thought to reduce the computational time used in the MPC. However, this approach has still a high computational cost.

Moreover, in 2009, [22] applied a two layer predictive controller that controls the formation of nonholonomic mobile vehicles was proposed. In their study, the authors considered that there are two sub-problems to be solved to fulfill the main goal: the trajectory control problem and the formation control problem. To solve the first sub-problem a nonlinear controller was proposed to control the robots' trajectory while a linear model predictive controller was proposed to solve the second sub-problem and control the robots' formation.

Considering the implementation of the approach using the NMPFC in a group of omnidirectional mobile robots, the next section will describe the control architecture used in this paper. In the following section, the nonlinear model predictive formation controller is presented. Furthermore, results from experiments with real robots are presented and discussed. The paper is then concluded in Section 4.

#### 2. Nonlinear model predictive formation controller

The nonlinear model predictive control is usually implemented in a centralized fashion. It holds full knowledge of the entire system and computes all the control inputs. A centralized control using a non-convex optimization scheme applied in large-scale interconnected systems, such as water distribution systems, traffic and power systems, manufacturing systems and economic systems, may be a too complex solution or not even feasible. With the quick development of communication networks, centralized control has been gradually replaced by distributed control such as in multi-robot systems and applications in manufacturing and process industries where multiple units cooperatively produce a good. In distributed control schemes, agents share information in order to improve closed-loop performance, robustness and faulttolerance [23]. In the approach described in this paper, the agents (robots) share their local measurements (states) and receive the other agents' states, computing a control input using a reduced order model of the formation system dynamics. The challenge in this case is to formulate a simpler and decentralized problem which leads to a behavior that is similar to the one obtained using a centralized approach [24].

The objective of this paper is to formulate a nonlinear model predictive formation controller (NMPFC) for a multi-robot systems formation control. The general structure of a coordinated multirobot system can be classified in three categories: distributed, centralized, or hybrid (partially distributed). These classifications are based on how the control signals of each robot are calculated. In this case, the control architecture is fully distributed [23].

The NMPFC's ability to create and maintain a formation is due to the fact that the cost functions used by the controllers of each robot in the team are coupled. The above mentioned coupling occurs when the teammates' states are used in the cost function of each robot's controller to penalize the geometry or the deviation from the desired objective. This means that the actions of each robot affect every other teammate. The optimization of a cost function that takes into account the target position and obstacle avoidance takes out the necessity of a path planner and a control loop that are usually separated in two different modules. Here there is no path planner, only the NMPFC. Each robot keeps the formation state (pose and speed of the robots in formation, and position and speed of any target that should be followed), updating them in each control loop. This information is received by the controller of each robot in the formation which in turn creates the formation geometry where the actions of each robot affect the other teammates. The NMPFC can be divided into two sub-blocks:

- Optimizer This sub-block uses an online numeric minimization method to optimize the cost function and generate the signals of optimal control. The resilient propagation (RPROP) method is used here, which guaranties quick convergence [25];
- *Predictor*—The predictor performs the state evolution of the robot itself, the teammates and the target based on pre-defined models. It uses a simplified dynamic model to emulate the robot's evolution. The velocities of the teammates and target are assumed to be constant and equal to the last known velocities during the entire prediction horizon. The obstacles (moving or static) are assumed to have zero velocities during the control loop and the evolution of the relative distance between the obstacle and the robot is predicted. The predictor also emulates the evolution of the target's merged state covariance matrix.

Fig. 2 illustrates the structure of the NMPFC used in this work, where  $U(k|k) = U(k) = \begin{bmatrix} v_{ref}(k) & vn_{ref}(k) & w_{ref}(k) \end{bmatrix}^T$  is the output control signal in the first prediction step,  $\hat{U}(k + i|k)$  with  $i = 0 \dots N_c - 1$  is the output control signal from the optimizer sent to the predictor, and  $\hat{P}(k + i|k)$  with  $i = 1 \dots N_p$  is the response of the predictor block to each  $\hat{U}(k + i|k)$ . Here, at an instant k, robot 1 (R<sub>1</sub>) sends its pose  $P_{R_1}(k) = \begin{bmatrix} x_{R_1}(k) & y_{R_1}(k) & \theta_{R_1}(k) \end{bmatrix}^T$  to the NMPFC. Furthermore, the NMPFC also receives the other robots' poses  $[P_{R_2}(k) \dots P_{R_N}(k)]$ , the position of the target t in the world frame  ${}^wP_t(k) = \begin{bmatrix} wx_t(k) & wy_t(k) \end{bmatrix}^T$  and the velocity of the target t in the world frame  ${}^wV_t(k) = \begin{bmatrix} wv_{xt}(k) & wv_{yt}(k) \end{bmatrix}^T$ . Fig. 2 also shows the block diagram of the proposed formation

Fig. 2 also shows the block diagram of the proposed formation control framework for robot  $R_1$  in a formation with N robots. The subscripted  $R_n$  is used to denote the robot n where  $1 \le n \le N$  and N is the total number of robots in formation and the subscripted t to denote the target. Each robot has an NMPFC, a cooperative target estimator (CTE) [26] and a real time data base (RTDB) communication application [27]. Other functions such as localization and the vision system are embedded in other software modules represented here as the block *Other Modules from Robot* 1. At each

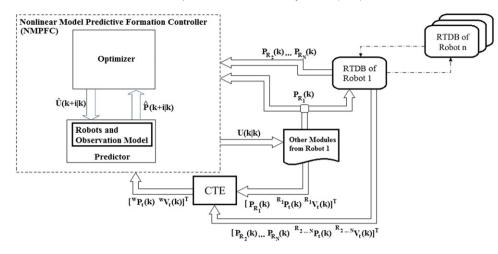


Fig. 2. Controller diagram.

instant k the robot  $R_1$  sends its pose  $(P_{R_1}(k))$  to the controller and to the RTDB to be shared with the formation. The robot also sends its pose ( $P_{R_1}(k)$ ), the position of the target in its local frame ( ${}^{R_1}P_t(k)$ ) and the velocity of the target in its local frame  $({}^{R_1}V_t(k))$  to the CTE. Then, the CTE, represented as a single block in Fig. 2, receives from the RTDB the pose, as well as the position and velocity of the target in the local frame of each other robot in formation, and also communicates locally to the NMPFC the information on the fused target position ( ${}^{w}P_{t}(k)$ ) and the fused target velocity ( ${}^{w}V_{t}(k)$ ), both in the world frame. An additional layer in communication using a real time data base (RTDB) shared memory makes it possible to convey information. Then, each robot writes its own pose and reads the teammates'. The NMPFC also receives the pose of each robot in formation ( $[P_{R_2}(k) \dots P_{R_N}(k)]$ ) from the robot's RTDB and then sends an output control signal U(k) to the robot (the tangential and normal components of linear velocity and angular velocity).

After receiving the states of the robot, teammates, obstacles and target, the controller's optimizer sub-block provides the control input  $\hat{U}(k + i|k)$ , in a limited control horizon, to the predictor sub-block, which then predicts the formation state evolution  $\hat{P}(k + i|k)$  for  $N_p$  steps (prediction horizons), and provides a cost value to the optimizer in accordance with  $\hat{U}(k+i|k)$ . The iterative minimization process is repeated in cyclic fashion. Finally, the control output in the first step U(k) is sent to the robot.

The robot's pose and velocity estimation is performed using a localization algorithm that uses data from the odometry, from a digital compass and from the omnidirectional camera. Then, using the omnidirectional camera to detect the white lines of the field combined with a map matching algorithm the robot is localized. During the robots' movement, the velocity is estimated also using the data from the odometry.

To achieve convergence in the formation, and hence cost function minimization, the NMPFC's predictor sub-block produces the evolution of the formation's behavior, as well as the behavior of the target's merged state and covariance matrix which is used by the NMPFC's optimizer and predictor sub-blocks for the cyclic minimization process. After processing the control calculations, the NMPFC sends the desired control output back to the robot (controller's reference velocities).

#### 2.1. The model

In a robot  $R_n$  (where  $1 \le n \le N$  and N is the total number of robots in the formation) the wheels' angular velocities data  $(\omega_{rR_n}(k) = [\omega_1(k) \ \omega_2(k) \ \omega_3(k)]^T)$  are given by the odometry and, therefore, the wheels' linear velocity is given by  $V_{rR_n}(k)$ 

=  $\begin{bmatrix} v_1(k) & v_2(k) & v_3(k) \end{bmatrix}^T = r \cdot \begin{bmatrix} \omega_1(k) & \omega_2(k) & \omega_3(k) \end{bmatrix}^T$ . Therefore, the robot's velocities can easily be found using the equation below:

$$\begin{bmatrix} v_{R_n}(k) \\ v_{R_n}(k) \\ w_{R_n}(k) \end{bmatrix} = (B)^{-1} \cdot \begin{bmatrix} v_1(k) \\ v_2(k) \\ v_3(k) \end{bmatrix}$$
(1)

with

$$B = \begin{bmatrix} \cos(\delta) & \sin(\delta) & d \\ -\cos(\delta) & \sin(\delta) & d \\ 0 & -1 & d \end{bmatrix} = \begin{bmatrix} \frac{\sqrt{3}}{2} & \frac{1}{2} & d \\ -\frac{\sqrt{3}}{2} & \frac{1}{2} & d \\ 0 & -1 & d \end{bmatrix}$$
(2)

where  $\delta = 30^{\circ}$ , resulting

$$(B)^{-1} = \begin{bmatrix} \frac{\sqrt{3}}{3} & \frac{\sqrt{3}}{3} & 0\\ \frac{1}{3} & \frac{1}{3} & -\frac{2}{3}\\ \frac{1}{3d} & \frac{1}{3d} & \frac{1}{3d} \end{bmatrix}.$$
 (3)

The omnidirectional mobile robot model used in the *Predictor* is a nonlinear simplified model that, when properly parameterized [28], is advantageous in order to reduce the computational load of each cycle of the control algorithm. This translates into the ability to use greater prediction horizons in the predictive controller, even in computers with modest specifications, keeping the cycle time control within the required limits. The model is initialized with the limitation of the motor's velocity by detecting saturation and proportionally scaling the other motors (which can be seen as an input constraint) [29]. Furthermore, the prediction of the wheels' velocities of robot  $R_n$  follows a first order discrete model, where

$$\begin{bmatrix} v_1(k) \\ v_2(k) \\ v_3(k) \end{bmatrix} = a \cdot \begin{bmatrix} v_1(k-1) \\ v_2(k-1) \\ v_3(k-1) \end{bmatrix} + (1-a) \cdot (B^T) \cdot \begin{bmatrix} v_{\text{ref}R_n}(k) \\ v_{n_{\text{ref}R_n}}(k) \\ w_{\text{ref}R_n}(k) \end{bmatrix}$$

Then, its result is once more inserted in Eq. (1) to be computed. Therefore, its state (pose  $(P_{R_n}(k))$  and velocity  $(V_{R_n}(k))$ ) are defined as

$$P_{\mathbf{R}_{n}}(k) = \begin{bmatrix} x_{\mathbf{R}_{n}}(k) & y_{\mathbf{R}_{n}}(k) & \theta_{\mathbf{R}_{n}}(k) \end{bmatrix}^{\mathrm{T}} V_{\mathbf{R}_{n}}(k) = \begin{bmatrix} v_{\mathbf{x}\mathbf{R}_{n}}(k) & v_{\mathbf{y}\mathbf{R}_{n}}(k) & w_{\mathbf{R}_{n}}(k) \end{bmatrix}^{\mathrm{T}}$$
(4)

and the simulation of the state evolution is given by

$$\begin{bmatrix} x_{R_n}(k) \\ y_{R_n}(k) \\ \theta_{R_n}(k) \end{bmatrix} = \begin{bmatrix} x_{R_n}(k-1) \\ y_{R_n}(k-1) \\ \theta_{R_n}(k-1) \end{bmatrix} + T \cdot \begin{bmatrix} v_{xR_n}(k) \\ v_{yR_n}(k) \\ w_{R_n}(k) \end{bmatrix}$$

with *T* as the time step and

$$\begin{bmatrix} v_{xR_n}(k) \\ v_{yR_n}(k) \\ w_{R_n}(k) \end{bmatrix} = \begin{bmatrix} \cos(\theta_{R_n}(k)) & -\sin(\theta_{R_n}(k)) & 0 \\ \sin(\theta_{R_n}(k)) & \cos(\theta_{R_n}(k)) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$
$$\cdot \begin{bmatrix} v_{refR_n}(k) \\ v_{refR_n}(k) \\ w_{refR_n}(k) \end{bmatrix}.$$

Taking into account the elements presented, the position  $P_t(k)$  and velocity  $V_t(k)$  of the target t (ball) in the world frame at an instant k is defined as

$$P_{t}(k) = \begin{bmatrix} x_{t}(k) & y_{t}(k) \end{bmatrix}^{T} \qquad V_{t}(k) = \begin{bmatrix} v_{xt}(k) & v_{yt}(k) \end{bmatrix}^{T}$$
(5)

where

$$\begin{cases} x_t(k) = x_t(k-1) + T \cdot (v_{xt}(k)) \\ y_t(k) = y_t(k-1) + T \cdot (v_{y_t}(k)) \end{cases}$$
(6)

and

$$\begin{cases} v_{xt}(k) = v_{xt}(k-1) \cdot B_{FC} \\ v_{yt}(k) = v_{yt}(k-1) \cdot B_{FC} \end{cases}$$
(7)

where  $B_{FC}$  is the ball friction coefficient.

The target's velocity unit vector is then defined as

$$\tilde{V}_{t}(k) = \begin{bmatrix} \tilde{v}_{x} t(k) & \tilde{v}_{y} t(k) \end{bmatrix}^{\mathrm{T}} = \frac{V_{t}(k)}{\|V_{t}(k)\|}.$$
(8)

The position of the target relative to the robot  $R_n$  at an instant k is defined as

$$P_{t}^{R_{n}}(k) = \begin{bmatrix} x_{t}^{R_{n}}(k) & y_{t}^{R_{n}}(k) \end{bmatrix}^{T}$$
(9)

where

.

$$\begin{cases} x_{t}^{R_{n}}(k) = x_{t}(k) - x_{R_{n}}(k) \\ y_{t}^{R_{n}}(k) = y_{t}(k) - y_{R_{n}}(k). \end{cases}$$
(10)

The unit vector which indicates the direction of the target with respect to the robot is defined as

$$\tilde{P}_{t}^{R_{n}}(k) = \begin{bmatrix} \tilde{x}_{t}^{R_{n}}(k) & \tilde{y}_{t}^{R_{n}}(k) \end{bmatrix}^{\mathrm{T}} = \frac{P_{t}^{R_{n}}(k)}{\|P_{t}^{R_{n}}(k)\|}.$$
(11)

The bearing of the target with respect to robot  $R_n$  is defined as

$$\theta_t^{R_n}(k) = \arctan 2(y_t^{R_n}(k), x_t^{R_n}(k)).$$
(12)

The poses of a robot  $R_n$  relative to its teammate  $R_j$  (where  $1 \le j \le NM$ , and *NM* is the total number of mates) are defined as

$$P_{R_n}^{R_j}(k) = \begin{cases} x_{R_n}^{R_j}(k) = x_{R_n}(k) - x_{R_j}(k) \\ y_{R_n}^{R_j}(k) = y_{R_n}(k) - y_{R_j}(k) \end{cases}$$
(13)

and with respect to an obstacle  $O_l$  (where  $1 \le l \le NO$ , and NO is the total number of obstacles), it is defined as

$$P_{R_n}^{O_l}(k) = \begin{cases} x_{R_n}^{O_l}(k) = x_{R_n}(k) - x_{O_l}(k) \\ y_{R_n}^{O_l}(k) = y_{R_n}(k) - y_{O_l}(k). \end{cases}$$
(14)

It is important to mention that in the obstacle's state evolution, all obstacles (moving or static) are considered as having zero

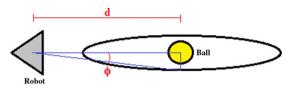


Fig. 3. Model of observation.

velocity at that time instant in order to reduce the computation load as the number of obstacles increases.

Finally, in order to model the evolution of the total amount of uncertainty with respect to the relative position between the robot and the target, a covariance model was created based on Fig. 3. This model depends on the type of camera used (such as omnidirectional mirror-camera, fish eye camera, normal direct cameras). Nevertheless, the model can easily be changed using the controller's code, allowing each robot to have a different sensor.

In the omnidirectional 5dpo robot camera, the point on the ground plane directly below the robot's catadioptric system center (also the robot's geometric center) is assumed to be the origin O of the coordinates for the model discussed in this sub-section. The target observation  $M_{R_n}$  is represented as a 2D vector  $[d_t, \phi]$ .  $d_t$ , where  $d_t \ge 0$ ,  $d_t \in \mathbb{R}$  is the distance to the target from O and  $\phi$ , where  $-\pi \le \phi \le +\pi$ ,  $\phi \in \mathbb{R}$  is the bearing of the target from the positive X axis of the robot. The covariance model of a robot  $R_n$  in the instant k is given by (15):

$$\Sigma_{\mathbf{R}_n}(k) = \begin{bmatrix} \sigma_{d_t}^2 & \rho \sigma_{d_t} \sigma_{\phi} \\ \rho \sigma_{\phi} \sigma_{d_t} & \sigma_{\phi}^2 \end{bmatrix}$$
(15)

where  $\sigma_{d_t}$  is the variance of the target's distance measurement  $d_t$ and  $\sigma_{\phi}$  is the variance of the target's bearing measurement.  $\rho$  is the correlation coefficient. It is assumed that both the measurements are uncorrelated and  $\rho = 0$ .

In the case of the 5dpo robots, an empirical observation covariance model (16) was created where the variance in the target distance is directly proportional to the distance squared and the variance in the target bearing is inversely proportional to the target distance. This observation model was validated with several experiments in which it was also possible to find the values of  $K_a$  and  $K_b$ :

$$\Sigma_{\mathbf{R}_n}(k) = \begin{bmatrix} K_a d_t^2 & 0\\ 0 & K_b \frac{1}{d_t} \end{bmatrix}.$$
 (16)

Furthermore, it is necessary to represent the observation covariance (16) in its canonical form in the Cartesian coordinates centered at *O* due to the need of ease up the covariances merging arising from the teammates. Therefore, the canonical representation of the covariance model in the direction of the target and in its perpendicular direction is given by (17):

$$\Sigma_{\mathbf{R}_{n}}^{\perp}(k) = \begin{bmatrix} K_{1}d_{t}^{2} & 0\\ 0 & K_{2}d_{t} \end{bmatrix} = \begin{bmatrix} \sigma_{x}^{2} & 0\\ 0 & \sigma_{y}^{2} \end{bmatrix}$$
(17)

where  $K_1 = K_a$  and  $K_2 = (K_b + K_a K_b)$  are constants of proportionality.

The covariance merging is performed using Smith and Cheeseman's formulation [30]. In the formation, each robot teammate covariance  $\Sigma_{R_j}^{\perp}(k)$  is also predicted. The teammate's predicted covariance is also rotated in the robot's frame and then merged as per the method presented in [30]. Therefore, if it is given *N* robots in a formation, then  $R_n$  is the robot predicting its formation covariances and the robots  $R_j$  are the teammate with  $1 \le j \le NM$ and NM = N - n are the number of teammate in formation. The merged covariances are given by

$$\Sigma_{\text{Merged}}^{\perp}(k) = ([\Sigma_{\text{R}_{n}}^{\perp}(k)]^{-1} + [\hat{\Sigma}_{\text{R}_{j=1}}^{\perp}(k)]^{-1} + \dots + [\hat{\Sigma}_{\text{R}_{j=NM}}^{\perp}(k)]^{-1})^{-1}$$

where  $\hat{\Sigma}_{R_j}^{\perp}(k)$  are the covariance rotated matrices of the teammates with respect to the robot  $R_n$ .

No noise was introduced in simulation experiments. Therefore, the means of observation estimates from teammates are identical while the uncertainty ellipse around each teammate's observation is formulated as per (17) for merging.

#### 2.2. The cost function during the presence of a target

The cost function of a NMPC (here NMPFC) represents the cost to be minimized by the predictive controller. It is typically associated with the dynamical change of the system (formation geometry) over time. Therefore, reducing the uncertainty of the target's localization and velocity estimates, while keeping the robots apart and assigning costs to the motion of the robots (for instance, to get closer to a ball). Therefore, the term (18a) of the cost function penalizes the total amount of uncertainty given by the merged covariance matrix  $\Sigma_{Merged}^{\perp}(k)$ . The term (18b) penalizes the distance between the target and the robot  $\|P_t^{R_n}(k)\|$ . To avoid collision, the penalization takes into account a threshold distance that the robot must maintain between it and the target ( $D_{val}$ ).

The function (18c) penalizes the difference between the angle of the robot in the world frame (the orientation of the robot in world frame) and the angle between the robot and the target, which will allow the robot to face the ball. In the case of the 5dpo mobile robot, it faces the target when its concave face (the kicking mechanism) is toward the target. The function  $\delta(\cdot)$  receives two angles as arguments and returns their difference scaled between  $-\pi$  and  $\pi$ . The following term will influence the robot's position with respect to the target's velocity vector. It penalizes if the robot is in the wrong position during the target's movement. Here, the  $P_{\text{val}}$  will change this position and it must have a value between 1 and -1. Note that this range of values can allow the robot to be in front of the ball, behind the ball or at its side.

The function (18e) is a potential function that penalizes the proximity between the robot and its available mates (NM). Here, the potential fields approach was used to create the mates avoidance term of the cost function. It is a modification of the previous version [31] and its weights change if the robot is too close to its mates. This is a negative linear function of distance. In the function, the given value where small distances are not penalized is  $D_M = 1.5$  m. Therefore, the robots must keep a relative distance between them greater than  $D_M$ . The function (18f) works in the same way as the previous function, although it is used here to avoid obstacles. While in the last function the second sum adds until the maximum number of available mates, this function sums all obstacles in the robot's sensor range (NO). Here,  $D_0 = 1.5$  m has the same purpose of  $D_M$  but regarding obstacles. The NMPFC deals adequately with constraints. Although it was considered avoiding collisions using an explicit state constraint, it was not taken this choice because it would slow down the optimization algorithm.

Finally, the term (18g) penalizes the control effort. In this last function, the variation in the output control signal is penalized instead of its absolute value. Penalizing the output control signal would create a steady-state error in non-zero velocities (for example when pursuing a moving target).

The final cost function (18) is a composition of seven terms. Nevertheless, it is important to remember that here  $| \cdot |$  denotes 1-norm for vector arguments and the absolute value for scalars as well as  $|| \cdot ||$  represents the euclidean norm. Taking into account all

the elements previously described, the weights given to each one of them, and a penalization term to the variation of control effort, the cost function that represents all this, embedded in all robots, is as follows:

$$J(N_1, N_p, N_c) = \sum_{i=N_1}^{N_p} \lambda_a \times |\det(\Sigma_{\text{Merged}}^{\perp}(k+i))|$$
(18a)

+ 
$$\sum_{i=N_1}^{N_p} \lambda_0 \times |(D_{\text{val}} - ||P_t^{R_n}(k+i)||)|$$
 (18b)

+ 
$$\sum_{i=N_1}^{N_p} \lambda_1 \times |\delta(\theta_{\mathbf{R}_n}(k), \theta_{\mathbf{t}}^{\mathbf{R}_n}(k+i))|$$
 (18c)

$$+\sum_{i=N_1}^{N_p} \lambda_2 \times |P_{\text{val}} + (\tilde{P}_t^{R_n}(k+i) \cdot \tilde{V}_t(k+i))|$$
(18d)

$$+\sum_{i=N_1}^{N_p}\sum_{j=1}^{NM}\lambda_3 \times \max\left(\left|1-\frac{\|P_{R_n}^{R_j}(k+i)\|}{D_M}\right|,0\right)$$
(18e)

$$+ \sum_{i=N_1}^{N_p} \sum_{l=1}^{NO} \lambda_4 \times \max\left( \left| 1 - \frac{\|P_{R_n}^{O_l}(k+i)\|}{D_0} \right|, 0 \right)$$
(18f)

$$+\sum_{i=1}^{N_c} \lambda_5 \times |\Delta U(k+i-1)|$$
(18g)

where  $N_1$ ,  $N_p$  are the predicted horizon limits in discrete time, such that  $N_1 > 0$  and  $N_2 \le 7$ .  $N_c = 2$  is the control horizon.  $\lambda_a$ ,  $\lambda_0$ ,  $\lambda_1$ ,  $\lambda_2$ ,  $\lambda_3$ ,  $\lambda_4$  and  $\lambda_5$  are the weights for each component of the cost function.  $\Sigma_{Merged}^{\perp}$  is the formation team's merged target observation covariance matrix.  $D_{val}$  is the threshold distance between the robot and the ball.  $P_{val}$  is the position coefficient which puts the robot around the ball in a determined position.  $\Delta U(k+i-1)$  is the variation of the control signals, where U(k) is the velocity vector of the robot's frame.

Several differences improve this work when compared to our previous one presented in [31]. They are as follows:

- There is a penalization function of the total amount of uncertainty of the target's perception, which allows the robots to be in the better position while converging or following a target.
- In the control effort penalization term, the 1-norm is used, which gives the controller more efficiency [32]. However, the disadvantage of 1-norm is its high nonlinearity. Given that it was adopted RPROP [25] and that it is a heuristic optimizer, it can handle the nonlinearities introduced by the use of the 1-norm.
- There was a modification on the obstacle avoidance function using a potential field approach.
- In this work, only one cost function works as a substitute for the two cost functions presented in [31], independent of the position it may assume in formation.
- Here the absence of target case was also considered.
- The results from this work proved to have an improved final convergence of the formation.

#### 2.3. The cost function during the target's absence

The case of the target's absence is an important special case to be considered. To address this issue, another cost function similar to the previous one was created. This cost function is used only in case of the absence of a target in which each robot has to follow a robot leader which in turn performs a search in a preset area using

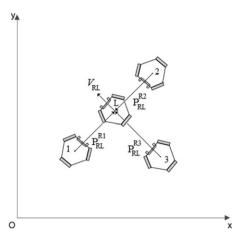


Fig. 4. Formation following a leader.

a normal reactive controller [33] with the path planner presented in [34]. Note that this cost function is used only by the follower robots.

The formation geometry, in this case, selects a fixed robot as the leader, while the other two robots become the followers. All the assumptions made for the last cost functions with respect to the target shall be made in this case with respect to the robot leader. An exception is the function (18a) due to the fact that the leader's pose is passed to the other robots (not estimated). Therefore, this cost function is a composition of six functions. The function (19a) penalizes the distance between a leader robot  $R_L$  and the follower robot  $\|P_{R_n}^{R_L}(k)\|$ . To avoid collision, the penalization also does not take into account a fixed distance that the robot must maintain between it and the leader robot  $(D_{val})$ .

The function (19b) penalizes the difference between the angle of the robot (a follower) in the world frame and the angle between the follower robot and the leader robot. This will make the robot face the leader while it is in movement. The last modification is in the function that will influence the robot's position with respect to the leader's velocity vector (19c) as can be seen in Fig. 4. It penalizes if the robot is in the wrong position. Here, the  $P_{val}$  will change this position and it must have a value between 1 and -1.

The terms (19d)–(19f) of this cost function are similar to the (18e)–(18g) terms of the cost function (18). Therefore, taking into account all the elements previously described, the weights given to each one of them, and a penalization term to the variation of control effort, the cost function that represents all this, embedded in both robots, is as follows:

$$J(N_1, N_p, N_c) = \sum_{i=N_1}^{N_p} \lambda_0 \times |(D_{\text{val}} - ||P_{R_L}^{R_n}(k+i)||)|$$
(19a)

$$+\sum_{i=N_1}^{N_p} \lambda_1 \times |\delta(\theta_{R_n}(k), \theta_{R_L}^{R_n}(k+i))|$$
(19b)

$$+ \sum_{i=N_1}^{N_p} \lambda_2 \times |P_{\text{val}} + (\tilde{P}_{R_L}^{R_n}(k+i) \cdot \tilde{V}_{R_L}(k+i))|$$
(19c)

$$+\sum_{i=N_{1}}^{N_{p}}\sum_{j=1}^{NM}\lambda_{3}\times \max\left(\left|1-\frac{\|P_{R_{n}}^{R_{j}}(k+i)\|}{D_{M}}\right|,0\right)$$
(19d)

$$+ \sum_{i=N_{1}}^{N_{p}} \sum_{l=1}^{NO} \lambda_{4} \times \max\left( \left| 1 - \frac{\|P_{R_{n}}^{O_{l}}(k+i)\|}{D_{0}} \right|, 0 \right)$$
(19e)

$$+\sum_{i=1}^{N_c} \lambda_5 \times |\Delta U(k+i-1)|.$$
(19f)

Table 1	
Einal woights for	the cost functi

Final weights for the cost function.	
λ	Weights
$\lambda_a$	505
$\lambda_0$	918
$\lambda_1$	297
$\lambda_2$	510
$\lambda_3$	500
$\lambda_4$	500
$\lambda_5$	5.00

#### 3. Results

Several simulations were made to validate the NMPFC controller. Furthermore, some experiments with real robots were also made in order to see the behavior of the group under communication, vision and localization problems. Each group has convergence and retaining formation experiments. For all results the same parameters were used. Nevertheless, some assumptions must be made such as follows:

- Distance between the robot and the ball or between the robot and the leader = 1.2 m.
- Velocity of the robots in formation or following leader = 1.5 m/s in simulations and 0.7 m/s in experiments.
- Velocity of the leader = 1 m/s in simulations and 0.5 m/s in experiments.
- The RPROP parameters were the same ones used in [31] with a maximum of 20 interactions.

The final values founded through the exhaustive simulations and experiments can be seen in Table 1.

Finally, the value of the weight  $\lambda_2$  was re-tuned compared to our previous work [31]. Analyzing the graphs of internal product and plot *XY* of the robots during the exhaustive simulations and experiments, we reached to an optimal value for this parameter. It is important to remember that this term is only active when the target (ball or robot leader) has a nonzero velocity.

#### 3.1. Simulations

Two simulations were done for formation convergence, one for the leader following the case with the target absent and one for keeping the formation case. In the simulations, the SimTwo simulator was used [35].

#### 3.1.1. Simulation 1: formation convergence

In the formation convergence, the target has zero velocity. Therefore, the fourth term in the cost function is equal to zero. Furthermore, without any obstacles the sixth term is also zero. The first simulation puts the robots initially as demonstrated in Fig. 5. The objective here is to make the robots converge toward the ball. The robots 1, 2 and 3, and the target's coordinates are (3.5, -1.8), (-3.5, -1.8), (0, 3.5) and (0, 0), respectively. In Fig. 5 plot *XY* of the robot's movement can be seen. Note here that the robot always stops facing the ball (with the carved part toward the ball). A graph with the distance between the robot and the ball as well as the minimization of the merged covariance's determinant can be seen in Fig. 6.

#### 3.1.2. Simulation 2: formation convergence

The second simulation places the robots initially as demonstrated in Fig. 7. The objective here is to push the robots to converge toward the ball departing from the coordinates (-5.5, 0), (-4.5, 0), (-3.5, 0) and (0, 0) for the robots 1, 2, 3 and the target, respectively. This environment was created aiming to observe if the robots can avoid collisions between them. In Fig. 7, plot XY of the robot's movement can also be seen. A graph with the distance between the robot as well as the minimization of the merged covariance's determinant can be seen in Fig. 8.

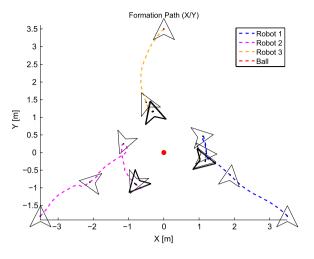


Fig. 5. Simulation 1: formation convergence-plot XY.

## 3.1.3. Simulation 3: the leader following

The last simulation of formation convergence positions the robots initially as demonstrated in Fig. 9. The objective here is to make the robots converge to the leader robot departing from the coordinates (4.3, -3.1), (4.3, 0), (4.3, 5.1) for the robots 2, 1 and 3, respectively, and keep a formation while following the leader robot. In this case, the target is not seen in the field, so robot 2 (as the leader robot) has an A\* path planner seen in [34] with a reactive controller [33] while the follower robots (robots 1 and 3) possess the second cost function presented in this study.

In Fig. 9, plot XY of the robot's movement and a graph with the distance between the robot and the robot leader are also presented. It also shows the graphs of the internal product between the leader and the other robots as well as the angle between them. The given  $P_{\text{val}}$  for robot 1 was  $P_{\text{val}} = 1$  and for robot 3 was  $P_{\text{val}} = 0$ . The internal product's graph shows here the convergence for these values. The abrupt changes in the internal product of the robots is explained by the re-orientation of the robot leader during the search. Note in Fig. 9 that the robot leader performs three big turns, or re-orientations, in its path (in coordinates (-4.3, -3), (-4.5, 3) and (4.5, 3), respectively). When the leader robot turns, the followers became oriented in 90 (°) with respect to the leader's orientation until they converge again, also explaining the "jumps" in these graphs.

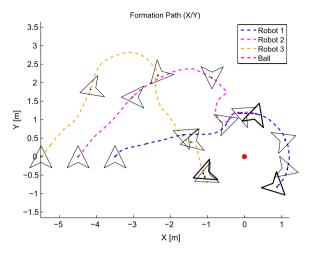


Fig. 7. Simulation 2: formation convergence-plot XY.

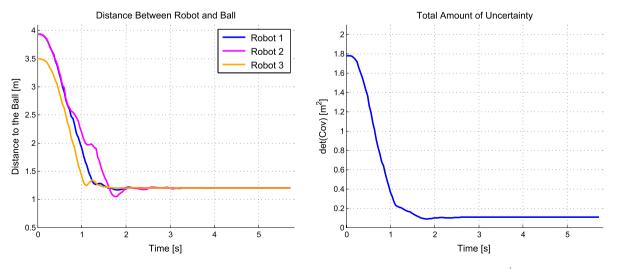
#### 3.1.4. Simulation 4: keeping formation

In this single simulation, the fourth term in the cost function is taken into account with the movement of the target. Nevertheless, without any obstacles the sixth term is zero. This simulation places the robots initially as demonstrated in Fig. 10. The objective here is for robots to keep following the ball in a straight trajectory. Robots 1, 2, 3 and the target's coordinates are (0, -1.5), (0, 1.5), (1.5, 0) and (0, 0), respectively. Then, a small impulse (kick) was given to the ball forcing it to possess a nonzero velocity. In Fig. 10 plot *XY* of the robot's movement can be seen. A graph with the distance between the robot and the ball and the minimization of the merged covariance's determinant can be seen in Fig. 11.

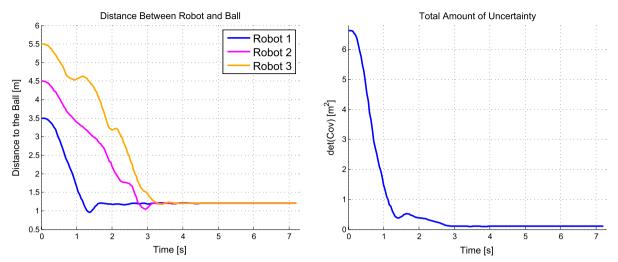
Fig. 11 also shows the graphs of the internal product between the robots and the ball as well as the angle between the robots and the ball's velocity vector. The given  $P_{val}$  for robots 1, 2 and 3 were  $P_{val} = 0$ ,  $P_{val} = 0$  and  $P_{val} = 1$ , respectively.

#### 3.2. Results of the experiments with real robots

A setup, to perform experiments with real robots, was created in order to analyze the behavior of three omnidirectional mobile robots with the NMPFC. An external computer connected to a router by a cable was needed in order to serve as a bridge of shared information through RTDB to all the robots, where the log could be collected from the robots. Therefore, to run the experiments



**Fig. 6.** Simulation 1: formation convergence—the distance between the robot and the determinant of  $\Sigma_{Merged}^{\perp}$ .



**Fig. 8.** Simulation 2: formation convergence—the distance between the robot and the determinant of  $\Sigma_{Merged}^{\perp}$ .

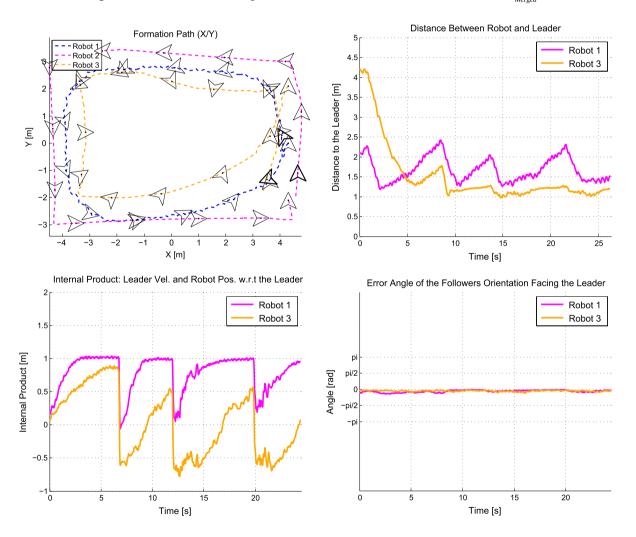


Fig. 9. Simulation 3: the leader following-plot XY and distance between the leader robot and the followers (top), the internal product between leader and followers and the error angle of the followers orientation facing the leader (bottom).

a workstation (Intel Core i7 3 GHz/Core with 8 Gb RAM) with Ubuntu 9.04 that runs said bridge was used. Each robot had a computer, a Notebook (Intel Dual Core 2 GHz/Core with 2 Gb RAM) with Ubuntu 9.04, running its own NMPFC, CTE and RTDB applications previously seen in Fig. 2. Finally, the experiments with real robots were executed in order to repeat the environment created in the simulations with two experiments in formation convergence, one for the leader following the case with the target absent and one for keeping the formation case. Videos from all experiments are attached to this paper which is available in

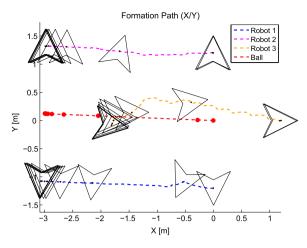
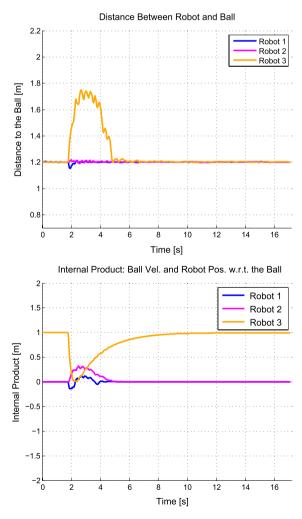


Fig. 10. Simulation 4: keeping formation-plot XY.

http://dx.doi.org/10.1016/j.robot.2013.07.005 to aid in the analysis of the robots' behavior during the tests.

## 3.2.1. Real experiment 1: formation convergence

The real experiments were conducted with robots number 1, 2 and 3. The first experiment placed the robots initially as demonstrated in Fig. 12. In this figure, plot *XY* of the robot's movement can also be seen. As it was in the first simulation, there is no obstacles in

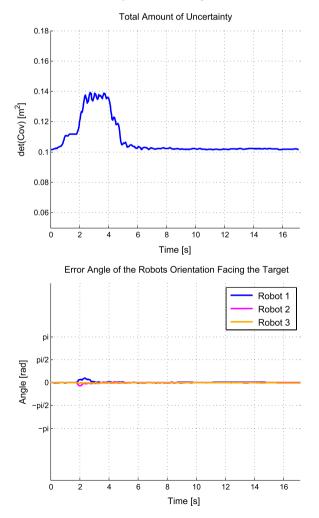


this experiment and the objective is to see the convergence toward a target placed in the center of the field. Robots 1, 2 and 3 are placed far from each other and their positions are (-3, 1.7), (0, -2) and (3, 1.7), respectively. All robots were 270° oriented in the world frame. The target's coordinates are (0, 0). In Fig. 13 the graph of the distance between the robot and the ball as well as the graph of the total amount of uncertainty (merged covariances) minimization can be seen. Video 1 shows robots' movement as presented in plot *XY*.

Note here that no collisions between the robots occur and that the robot always stops while facing the ball (with the carved part toward the ball) as shown in the simulations. As it can be seen, the ball "jumps" from one coordinate to another because the formation chooses the "best" ball amongst the balls' measurement which come from all three robots. Nevertheless, the robots move in a perfect circle around the ball while trying to minimize the covariance. That is explained by the fact that even if the best ball changes, or "jumps" from one coordinate to another, the total cost of these terms (covariance and distance) are kept very similar as it can be seen in Fig. 13. However, the formation converges successfully.

#### 3.2.2. Real experiment 2: formation convergence

The second experiment places the robots initially at the coordinates (2, 0), (3, 0), (4, 0) and (0, 0) for robots 1, 2, 3 and the target respectively, as demonstrated in Fig. 14. The objective here is to observe the robots converging to the ball avoiding collisions between them. Similarly to the second pair of simulations, the robots



**Fig. 11.** Simulation 4: keeping formation–distance between the robot and the ball and the determinant of  $\Sigma_{Merged}^{\perp}$  (top), the internal product between the robots and the ball and the error angle of the robots orientation facing the target (bottom).

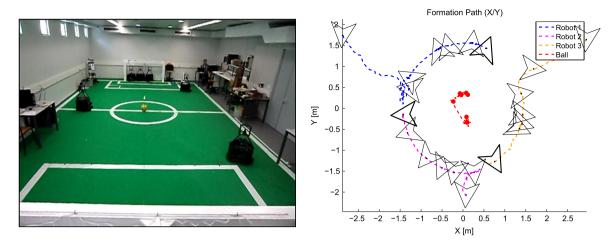


Fig. 12. Real experiment 1: formation convergence.

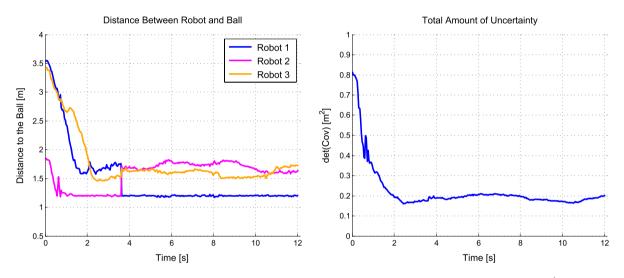


Fig. 13. Real experiment 1: formation convergence—the distance between the robot and the ball and the determinant of  $\Sigma_{Merged}^{\perp}$ .

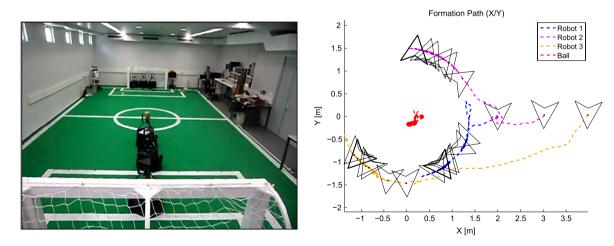


Fig. 14. Real experiment 2: formation convergence.

are placed in a horizontal line to increase the difficulty in the convergence forcing the robots to avoid each other. Video 2 shows the robots' movement successfully converging toward the target while avoiding collision between them.

In Fig. 15, a graph with the distance between the robot and the ball as well as the graph of the total amount of uncertainty (merged

# covariances) minimization can also be seen. Note that this time, there is no "jump" on the "best" ball.

## 3.2.3. Real experiment 3: the leader following

This experiment, like the leader following simulation, placed the robots initially as demonstrated in Fig. 16. The objective here

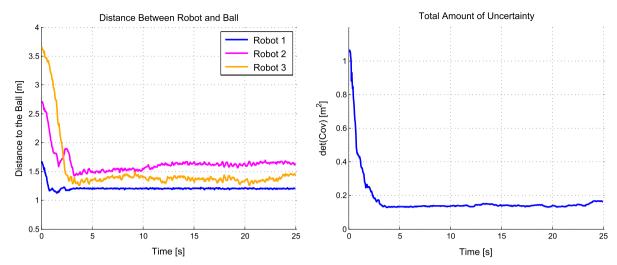


Fig. 15. Real experiment 2: formation convergence—the distance between the robot and the ball and the determinant of  $\Sigma_{\text{Merged}}^{\perp}$ .



Fig. 16. Real experiment 3: the leader following.

is to converge the two follower robots toward the leader robot departing from the coordinates (3, -2), (3, 0), (3, 2) for robots 1, 2 and 3, respectively. The follower robots must also keep a formation while following the leader.

Therefore, robot 1 (as the leader robot) has an  $A^*$  path planner with a reactive controller while the follower robots (robots 2 and 3) have the second cost function presented in this paper. In Fig. 17 plot *XY* of the robot's movement as well as a graph with the distance

between the follower robots and the robot leader can be seen. Video 3 shows the robots' movement as presented in plot *XY*.

Fig. 18 shows the graphs of the internal product between the leader and the other robots as well as the angle between them. Finally, the given value for  $P_{val}$  for robots 2 and 3 were  $P_{val} = -1$  and  $P_{val} = 0$ , respectively. Similarly to the simulations and despite the correct orientation toward the leader robot, the followers have trouble in converging the internal product due to the reasons previously explained. The abrupt changes in the robots' internal product are also explained by the same reasons demonstrated in the simulation of this experiment.

#### 3.2.4. Real experiment 4: keeping the formation

A last experiment was executed to perform formation maintenance with real robots. As the ball has a nonzero velocity, the fourth term in the cost function is taken into account. The real experiment consisted of pushing the ball in a straight line with the help of a stick to emulate a small kick. The robots 1, 2, 3 and the target's initial coordinates are (0, 1.5), (0, -1.5), (-1.5, 0) and (0, 0), respectively, as demonstrated in plot XY of the robot's movement in Fig. 19. Video 4 shows the robots' movement as presented in plot XY.

In the formation, each robot has, with a small amount of errors in the observation, its own measurement of the target in the world's frame. During the formation, this information is exchanged and a "best ball" is chosen from all the measurements that come

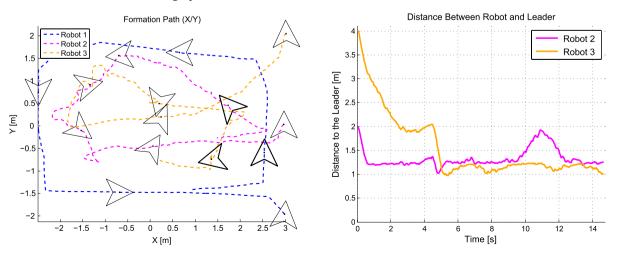


Fig. 17. Real experiment 3: the leader following-plot XY and the distance between the leader robot and the followers.

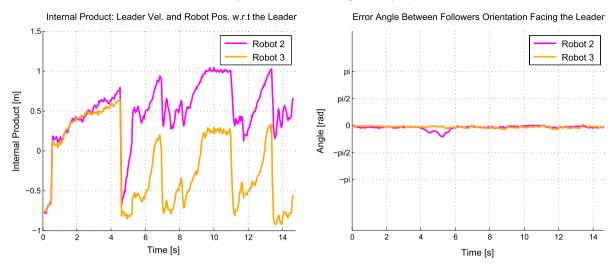


Fig. 18. Real experiment 3: the leader following-the internal product between the leader and followers and the error angle of the followers orientation facing the leader.

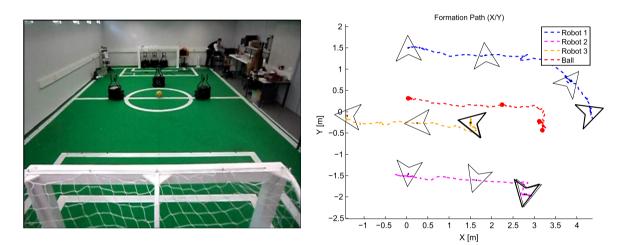
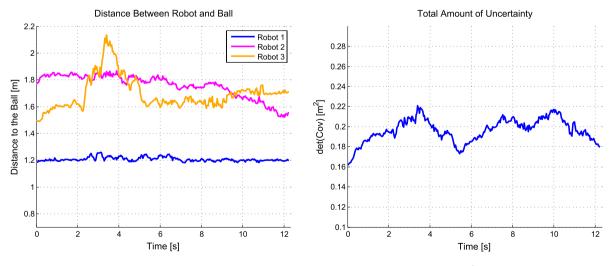


Fig. 19. Real experiment 4: keeping the formation.



**Fig. 20.** Real experiment 4: keeping the formation–plot *XY* and the determinant of  $\Sigma_{\text{Merged}}^{\perp}$ .

from the robots. As a "best ball" is chosen between the measured balls, the position of this final ball can create, along with small errors in the localization, differences in the distances between the robots and the ball as it can be seen in plot *XY* and in Fig. 20 that shows the distance between the robots and the ball and the graph

of the total amount of uncertainty (merged covariances) minimization.

Finally, in Fig. 21 the graphs of the internal product between the robots and the ball as well as the angle between the robots and the ball's velocity vector can be seen. The same values of  $P_{val}$  for robots

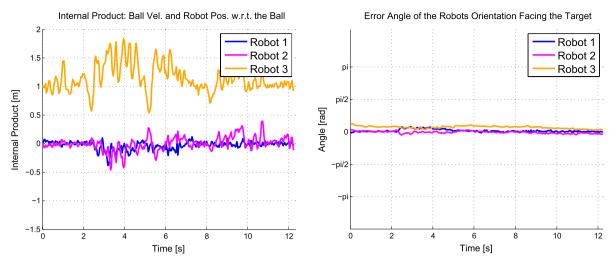


Fig. 21. Real experiment 4: keeping the formation-the internal product between the robots and the ball and the error angle of the robots orientation facing the target.

1, 2 and 3 used in the corresponding simulation were used in this experiment.

#### 4. Conclusion

This paper had the main objective to present a new nonlinear model predictive controller used in formation control of multirobot systems, here called a nonlinear model predictive formation controller (NMPFC). The NMPFC was implemented in order to converge a group of mobile robots toward a desired target and also to maintain the formation during the target's movement. Furthermore, a methodology to empirically find the initial values for the weights of the NMPFC cost function was presented. Finally, the case of the absence of a target was considered too, choosing a fixed leader robot in this case and using a second cost function to follow the leader robot. The details of the controller structure as well as a mathematical analysis of the formation model were presented.

This paper presented several novel contributions introduced by this work in formation control using a nonlinear model predictive controller, such as the distributive architecture to control robots in formation; a generic cost function for penalization of nondesirable behaviors of the formation when following an observed and noncontrolled target; the minimization of a merged covariances of the target perception in the cost function; and the controller's robustness despite vision and localization problems present in real robots environments.

The results also showed the influence of the vision system in the controllers efficiency during the formation keeping experiments. Small errors in the ball detection and localization are reflected in the calculation of the distance between the robot and the target and in the covariance minimization. Nevertheless, the controller was successful in converging the robots to the desired pose, minimizing the total amount of uncertainty while avoiding mates and setting the correct pose for all robots. Both convergence and keeping the formation were such that the total amount of uncertainty in the target's perception was minimized. Regarding the experiments without a target, the follower robots were successful in converging toward the leader and keeping the formation while the leader robot was moving.

It can be concluded that the NMPFC controller demonstrated a good performance in formation control of multi-robot systems. It could be implemented in different types of robots and penalize several non-desirable behavior of the formation with the same generic structure. Nonlinearities could be included in the prediction model such as the total amount of uncertainty in the target's perception which in turn gave relevance to the requirements imposed by target localization and/or tracking. Furthermore, energy costs, avoidance of obstacles, uncertainties and formation characteristics were considered in a single optimization problem. Nevertheless, among the disadvantages, the NMPFC still possesses reasonable computational costs in the system's processing. Finally, there is no guarantee of global minimization of the cost function during the optimization process. The stability analysis was not considered in this study as well. Nevertheless, the system is BIBO stable, for the robot's velocity was limited on 0.7 m/s where it could achieve up to 2 m/s for safety reasons.

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